A continuous-time optimal control approach based on Pontryagin's Maximum Principle with chance constraints

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Summary



Introduction: continuous-time optimal control with chance constraints

- 2 Writing the optimal control problem
- Writing the Hamiltonian and the ODE system
- Problem formulation
- 5
- Application to reference trajectory planning problem





Introduction





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Introduction

- Continuous-time optimal control with chance constraints to handle uncertainty
- Chance constraints guarantee a threshold of performance α of satisfaction
- We can derive a deterministic equivalent formulation in SOCP (second-order conic programming) [Prékopa, 2013]
- Comparison:
 - Solving the optimal control problem as a nonlinear optimisation problem with integral cost function [Valli et al., 2024]
 - Solving an ODE system as a two-point boundary value problem
- Application to reference trajectory planning generation for autonomous vehicles



Writing the optimal control problem





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Problem setup

- Let $n, m \in \mathbb{N}$ be dimensions of state and control vectors respectively $z(t) \in \mathbb{R}^n$, $u(t) \in \mathbb{R}^m$. Let $t_f \in \mathbb{R}, t_f \ge 0$ the final time.
- Integrand $I : \mathbb{R}^n \times \mathbb{R}^m \mapsto \mathbb{R}$, Integral cost function $J : \mathbb{R}^m \to \mathbb{R}$, Controls $\mathbf{u} = (u(t))_{t \in [0, t_f]}$ and states $\mathbf{z} = (z(t))_{t \in [0, t_f]}$

Cost function

$$J(\mathbf{u}) = \int_0^{t_f} I(z(t), u(t)) \, dt$$



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(1)

Optimisation problem

- Let α ∈ [0, 1]
- Control-state equation: $f : \mathbb{R}^n \times \mathbb{R}^m \to \mathbb{R}^n$,
- Random vector $a \sim \mathcal{N}(\mu, \Sigma)$, with $\mu \in \mathbb{R}^n$ the mean vector and $\Sigma \in \mathbb{R}^{n \times n}$ the covariance matrix, $b \in \mathbb{R}$

Optimisation problem with chance constraint

$$\min_{\mathbf{u}} \quad J(\mathbf{u})$$

s.t.
$$\frac{dz(t)}{dt} = f(z(t), u(t))$$
$$\mathbb{P}(a^{\mathsf{T}} z(t) \le b) \ge \alpha$$

(2)



Chance constraint reformulation

 Thanks to [Prékopa, 2013], the chance constraint is equivalent to a second-order conic programming (SOCP) constraint

Chance constraint

$$\mathbb{P}(\boldsymbol{a}^{\mathsf{T}}\boldsymbol{z}(t) \le \boldsymbol{b}) \ge \boldsymbol{\alpha} \Longleftrightarrow \boldsymbol{\mu}^{\mathsf{T}}\boldsymbol{z}(t) + \boldsymbol{F}^{-1}(\boldsymbol{\alpha}) \|\boldsymbol{\Sigma}^{1/2}\boldsymbol{z}(t)\|^{2} \le \boldsymbol{b}$$
(3)

with

- *F*(·) the cumulative distribution function (CDF) of the standard normal distribution *N*(0, 1).
- || · || the Euclidean norm



Writing the Hamiltonian





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Path constrained optimisation problems for nonlinear dynamic systems

From [Bryson, 2018], chapter 3.11, let

Constraint on function of the state variable

$$\mathbf{S}(\mathbf{z}(t)) := \boldsymbol{\mu}^{\mathsf{T}} \mathbf{z}(t) + \boldsymbol{F}^{-1}(\alpha) \mathbf{z}(t)^{\mathsf{T}} \boldsymbol{\Sigma} \mathbf{z}(t) - \mathbf{b}$$
(4)

Inequality constraint on function of the state variables only $S(z(t)) \leq 0$

Let

- $\lambda(t) \in \mathbb{R}^n$ the costates associated to z(t)
- $\eta(t) \in \mathbb{R}^n$, $\eta(t) \ge 0$ the time-dependent Lagrangian multipliers associated to S(z(t))



Time-dependent Lagrangian multipliers

• Time-dependent Lagrangian multipliers $\eta(t)$ are defined such as

Time-dependent Lagrangian multipliers

$$\begin{cases} \eta(t) = 0 & \text{if } S(z(t)) < 0 \\ \eta(t) > 0 & \text{if } S(z(t)) = 0 \end{cases}$$

Remark

Depending on the problem studied, discontinuities may appear at constraint saturation, leading to singular arcs [Bryson, 2018]



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q-th order state variable inequality constraint

- To control the system at constraint saturation S(z(t)) = 0, we need to find q ∈ N as the q − th time derivative of the constraint S(z(t)) depends explicitly on the command u(t).
- The order q is fixed such as it exists g : ℝⁿ × ℝ^m → ℝⁿ verifying the following condition:

q-th order state variable inequality constraint

$$\frac{d^{(q)}S(z(t))}{dt^{(q)}} = g(z(t), u(t))$$
(6)



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Tangency conditions

• The following condition must be checked for the command *u*(*t*) to be optimal

Tangency conditions

$$\frac{d^{(q)}S(z(t))}{dt^{(q)}} = 0 \quad \text{if } S(z(t)) = 0$$

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(7)

Hamiltonian formulation

• The Hamiltonian writes as

Hamiltonian

$$H(z(t), u(t), \lambda(t), \eta(t)) = I(z(t), u(t)) + \lambda^{T}(t) \cdot f(z(t), u(t))$$

$$+ \eta(t)^{T} \cdot \frac{d^{q}S(z(t))}{dt^{q}}$$
(8)



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Problem formulation





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Euler-Lagrange equations

 The Euler-Lagrange equations give ordinary differential equations to determine the costates λ(t)

Euler-Lagrange equations for costates $\lambda(t)$

$$\frac{d\lambda(t)}{dt} = -\frac{\partial H(z(t), u(t), \lambda(t), \eta(t))}{\partial z(t)}$$
(9)



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Transversality conditions and optimal command

• In our problem, there is no constraint at final time, therefore

$$\lambda(t_f) = 0 \tag{10}$$

• The optimal command $u^*(t)$ is obtained by

Optimal command $u^*(t)$

$$u^{*}(t) = \operatorname{argmin}_{u_{\min} \le u(t) \le u_{\max}} H\left(z(t), u(t), \lambda(t), \eta(t)\right)$$
(11)

It verifies the condition



Two-Point Boundary Value Problem (TPBVP)

• Finally, we obtain the two-point boundary value problem such as

TPBVP schema

$$\begin{array}{c} z(0) \\ \hline \lambda(0)? \end{array} \end{array} \left\{ \begin{array}{c} \frac{dz(t)}{dt} = f(z(t), u(t)) \\ \frac{d\lambda(t)}{dt} = -\frac{\partial H(z(t), u(t), \lambda(t), \eta(t))}{\partial z(t)} \\ \hline \lambda(t_f) = 0 \end{array} \right.$$
(13)



$\lambda^*(0)$ and shooting method

• Therefore, the control is determined by optimal initial values

Optimal initial values $\lambda^*(0)$

 $\lambda^*(0) = \operatorname{argmin} \|\lambda(t_f)\|$

- (14)
- Classical approach to solve this problem is to use the shooting method [Morrison et al., 1962]
- In our application, we use Levenberg-Marquardt algorithm [Gavin, 2019] with an estimation *λ*(0) as starting point, obtained by reversing the system (13) using results of our previous work [Valli et al., 2024] with costates *λ*(*t_f*) = 0. We use GEKKO optimisation solver [Beal et al., 2018].



Application to trajectory planning problem





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Trajectory planning I

• We represent the vehicle controlled (*the ego vehicle*) by its Cartesian coordinates.

Command u(t) and state z(t)

$$u(t) = \begin{pmatrix} j_t \\ \omega_t \end{pmatrix}$$
(15) $z(t) = \begin{pmatrix} x_t \\ y_t \\ \theta_t \\ v_t \\ a_t \end{pmatrix}$ (16)

- j_t is the jerk, ω_t the angular velocity
- (x_t, y_t) the Cartesian coordinates, θ_t the heading angle of the ego vehicle, v_t the linear speed and a_t the linear acceleration



Trajectory planning II

• The control-state relationship is given by :

$$\frac{dz(t)}{dt} = f(z(t), u(t)) = \begin{pmatrix} v_t \cos(\theta_t) \\ v_t \sin(\theta_t) \\ \omega_t \\ a_t \\ j_t \end{pmatrix}$$
(17)



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30



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Objective function

• The waypoints $(x_t^{wp}, y_t^{wp}, \theta_t^{wp})_{t \ge 0}$ corresponds to the centre lane of the road, v_r the recommended linear speed

Objective function

$$\int_{0}^{t_{f}} \mathbf{w}'_{x}(t) \left(\frac{x_{t}}{x_{t}^{wp}}-1\right)^{2} + \mathbf{w}'_{y}(t) \left(\frac{y_{t}}{y_{t}^{wp}}-1\right)^{2} + \mathbf{w}'_{h}(t) \left(\frac{\theta_{t}}{\theta_{t}^{wp}}-1\right)^{2}$$
(18)
+ $\mathbf{w}'_{v} \left(\frac{v_{t}}{v_{r}}-1\right)^{2} + \mathbf{w}'_{a} \cdot a_{t}^{2} + \mathbf{w}'_{\omega} \cdot \omega_{t}^{2} + \mathbf{w}'_{j} \cdot j_{t}^{2}$
+ $\mathbf{w}_{p} \cdot P(x_{t}^{tgt}, y_{t}^{tgt}, x_{t}, y_{t}) dt$



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Adaptive Cruise Control (ACC) feature

• The ACC feature [Liu et al., 2017] is modelled by

Adaptive Cruise Control

$$P(x_t^{tgt}, y_t^{tgt}, x_t, y_t) =$$

$$e^{-\left(\frac{(x_t^{tgt} - x_t)^2 + (y_t^{tgt} - y_t)^2}{2}\right) \left(1 + \operatorname{erf}\left(\frac{\operatorname{sign}(x_t^{tgt} - x_t)\sqrt{(x_t^{tgt} - x_t)^2 + (y_t^{tgt} - y_t)^2}}{\sqrt{2}}\right)\right)$$
(19)

With

$$\forall x \in \mathbb{R} \quad \operatorname{erf}(x) = \frac{2}{\sqrt{\pi}} \int_0^x e^{-t^2} dt$$
 (20)



Chance constraints on target distance

• Uncertainty on target vehicle position:

$$x_t^{tgt} \sim \mathcal{N}(\mu_{x_t}, \sigma_{x_t}), y_t^{tgt} \sim \mathcal{N}(\mu_{y_t}, \sigma_{y_t})$$
(21)

Equivalent constraints

From [Valli et al., 2024]

$$\mathbb{P}(|\mathbf{x}_t - \mathbf{x}_t^{tgt} + \mathbf{y}_t - \mathbf{y}_t^{tgt}| \ge \mathbf{d}_{min}) \ge \alpha \iff (22)$$

$$x_t + y_t \le \mu_{x_t} + \mu_{y_t} + d_{min} + \sqrt{\sigma_{x_t}^2 + \sigma_{y_t}^2 F_N^{-1}(\alpha/2)}$$
(23)

$$x_t + y_t \ge \mu_{x_t} + \mu_{y_t} - d_{\min} + \sqrt{\sigma_{x_t}^2 + \sigma_{y_t}^2} F_N^{-1} (1 - \alpha/2)$$
(24)



Experiments setup

Parameter	Function	Value
Vr	Reference linear speed	12 <i>m</i> .s ⁻¹
d _{min}	Minimum distance between vehicles	5 m
V _{max}	Maximum linear speed	40 <i>m</i> . <i>s</i> ⁻¹
ω _{max}	Maximum angular speed	$\frac{\pi}{6} s^{-1}$
a _{max}	Maximum acceleration	2 m.s ⁻²
j _{max}	Maximum jerk	0.6 <i>m.s</i> ⁻³

Table: Parameters' values for urban driving scenarios during the simulation.





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Algorithm Solving the continuous-time optimal control problem

- 1: Initialize z(0) initial state, t_f final time
- 2: **Solve** the optimal control problem using GEKKO solver starting from initial state z(0)
- 3: return $(z^{GEKKO}(t), u^{GEKKO}(t))_{[0,t_f]}$
- 4: **Reverse integration** of the TPBVP starting from $(z^{GEKKO}(t_f), \lambda(t_f) = 0)$
- 5: return $(\tilde{z}(0), \tilde{\lambda}(0))$
- 6: **Optimise** the initial costates by Levenberg–Marquardt algorithm applied on the TPBVP starting from $(z(0), \tilde{\lambda}(0))$
- 7: return $\lambda^*(0)$
- 8: Forward integration of the TPBVP
- 9: **return** $(z^{Pontryagin}(t), u^{Pontryagin}(t))_{[[0,t_f]]}$



Trajectory comparison



Optimal Commands



Constraint violations

• Quantity $d_{min} - |x_t^{tgt} - x_t + y_t^{tgt} - y_t|$



Conclusion

- Pontryagin solver achieves smoother command and tighter constraint handling than direct methods used by GEKKO solver
- Better minimise the cost function, but finding initial conditions can be complex
- Further perspectives: study the impact of approximations on the method (derivative of sign(·), choice of ODE solver, choice of optimisation technique); extend to higher time horizons; apply the approach to other optimal control problems





Thank you !





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Annexes





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Annex I : Transversality conditions

- Transversality conditions on the costates λ(t_f) depend on the constraints at final time t_f.
- Let Ψ : ℝⁿ → ℝⁿ represents the equality constraints on the final state such as Ψ(z(t_f)) = 0 and ν ∈ ℝⁿ the Lagrange multipliers associated.
- Let $\Phi(t_f) \in \mathbb{R}$ the terminal cost function such that

$$J(\mathbf{u}) = \int_0^{t_f} l(z(t), u(t)) \, dt + \Phi(t_f)$$
(25)

Transversality conditions

$$\lambda(t_f) = \frac{\partial}{\partial z(t_f)} (\Phi(t_f) + \nu^T \Psi(t_f))$$
(26)



Annex II : Numerical simulation I

- Time horizon: T = 4 s, time step $\Delta t = 0.04 s$
- Driving along the road, straight line $(\forall t \in \mathbb{R}^+ \ y_t = 0, \theta_t = 0)$





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Annex II : Numerical simulation II

Reverse integration

$$\tilde{z}(0) = \begin{pmatrix} -1.662\\0\\0\\14.840\\-1.631 \end{pmatrix}$$
(29) $\tilde{\lambda}(0) = \begin{pmatrix} -4.546\\0\\0\\-8.242\\-16.277 \end{pmatrix}$ (30)



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Annex II : Numerical simulation III

Levenberg–Marquardt optimisation

$$\lambda^*(0) = \begin{pmatrix} 0.572 \\ -9.194 * 10^{-17} \\ 1.460 * 10^{-16} \\ 0.959 \\ 0.533 \end{pmatrix}$$



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(31)

Annex II : Optimal cost

Numerical integration using Simpson's method

Optimal cost for GEKKO solver

$$J_{GEKKO}^{*}: \int_{0}^{t_{f}} I(z^{GEKKO}(t), u^{GEKKO}(t)) dt = 8.90$$
(32)

Optimal cost for Pontryagin solver

$$J_{\text{Pontryagin}}^*: \int_0^{t_f} I(z^{\text{Pontryagin}}(t), u^{\text{Pontryagin}}(t)) dt = 4.91$$
(33)

